

COMPARATIVE STUDY OF DENSITY-BASED VS. PRESSURE-BASED SOLVERS FOR SUPERSONIC FLOW

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GOAL OF THE PROJECT

- Project EULER: build a sounding rocket to reach 30k ft (\approx 9km)
- Supersonic!
- What solver to use for CFD?
- Opportunity for real-world validation



- **rhoPimpleFoam:** *pressure*-based compressible and transient solver
- **rhoCentralFoam:** *density*-based compressible and transient solver

The logo for OpenFOAM, featuring the word "Open" in black, a blue downward-pointing triangle, and the word "FOAM" in black, all on a white background.

Open  FOAM

Conservation of mass (continuity), momentum, and energy:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho U) = 0, \quad (1)$$

$$\frac{\partial}{\partial t}(\rho U) + \nabla \cdot (\rho U \otimes U) + \nabla p - \nabla \cdot \sigma = S, \quad (2)$$

$$\frac{\partial}{\partial t} E + \nabla \cdot (UE + Up) - \nabla \cdot \dot{q} - \nabla \cdot (U\sigma) = Q. \quad (3)$$

■ Pressure-based solvers:

- ▶ Solve the momentum equation for U
- ▶ Derive *pressure equation* from continuity and momentum equations
- ▶ Solve pressure equation for p
- ▶ *Correct* the velocity field with the pressure field

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- ▶ Diffuse shocks
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- ▶ Use equations of state to obtain p
- ▶ Shocks are explicitly considered when solving equations
- ▶ Make assumptions about shock speeds

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■ In general, we expect:

- ▶ Sharp shocks
- ▶ Shocks are conserved over time

COMPARISON 1: SUPERSONIC FLOW PAST WEDGE

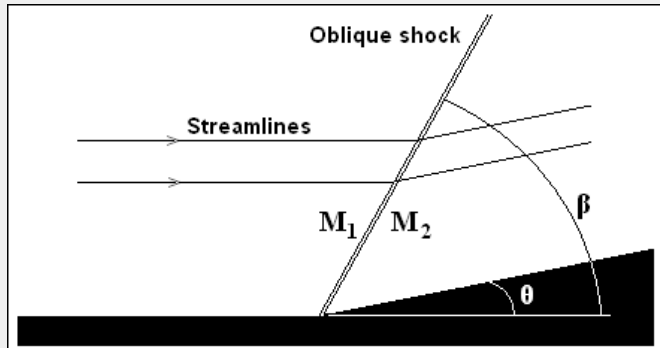


Figure 1: An illustration of the wedge problem (Source: Wikimedia Commons)

COMPARISON 1: SUPERSONIC FLOW PAST WEDGE

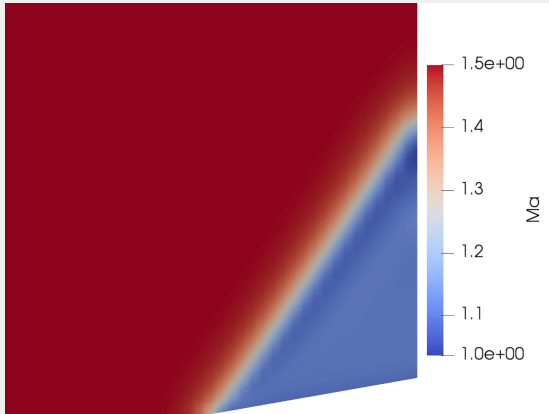


Figure 2: rhoPimpleFoam's solution

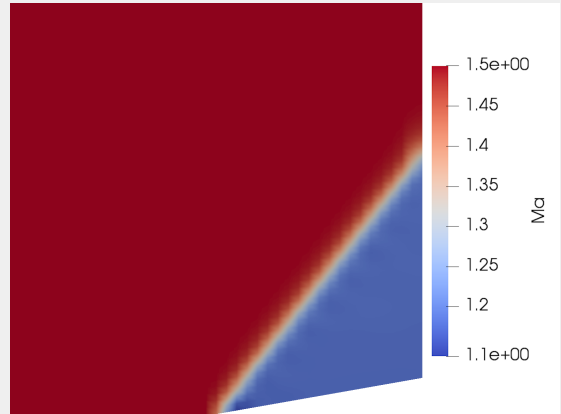


Figure 3: rhoCentralFoam's solution

COMPARISON 1: SUPERSONIC FLOW PAST WEDGE

Table 1: Results from the rhoPimpleFoam solver

θ	M_1	β	Rel. error	M_2	Rel. error	p_2/p_1	Rel. error
10	1.5	54	-4.73%	1.115618327	0.11%	1.666173008	0.00%
	2	39.5	0.47%	1.641311905	0.05%	1.707707792	0.07%
20	2	52	-2.66%	1.212560159	0.19%	2.842354736	-0.02%
	3	39	3.27%	1.988981188	-0.26%	3.798757552	0.73%

Table 2: Results from the rhoCentralFoam solver

θ	M_1	β	Rel. error	M_2	Rel. error	p_2/p_1	Rel. error
10	1.5	52	-8.25%	1.180810638	5.96%	1.576529862	-5.38%
	2	38.5	-2.07%	1.690511905	3.05%	1.658893471	-2.79%
20	2	49.5	-7.34%	1.331521595	10.02%	2.641398152	-7.09%
	3	37.5	-0.70%	2.127863366	6.71%	3.58902854	-4.83%

■ **rhoPimpleFoam** (pressure-based):

- ▶ Diffuses shock waves
- ▶ Diffusion gets worse further downstream
- ▶ Has overshooting
- ▶ Predicts slope fairly well despite diffusion
- ▶ Predicts values before/after shocks extremely well ($< 1\%$ error)

■ **rhoCentralFoam** (density-based):

- ▶ Resolves very sharp shocks
- ▶ Preserves shocks effectively
- ▶ No overshooting
- ▶ Not always as accurate at predicting shock slope
- ▶ Presents much larger errors when predicting values before/after shock (up to 10%! error)

- 1-D geometry
- Setup is a standard Riemann problem:

$$\begin{pmatrix} p_L \\ U_L \\ \rho_L \end{pmatrix} = \begin{pmatrix} 1.0 \\ 0.0 \\ 1.0 \end{pmatrix}; \quad \begin{pmatrix} p_R \\ U_R \\ \rho_R \end{pmatrix} = \begin{pmatrix} 0.1 \\ 0.0 \\ 0.125 \end{pmatrix} \quad (4)$$

COMPARISON 2: SOD'S SHOCK TUBE

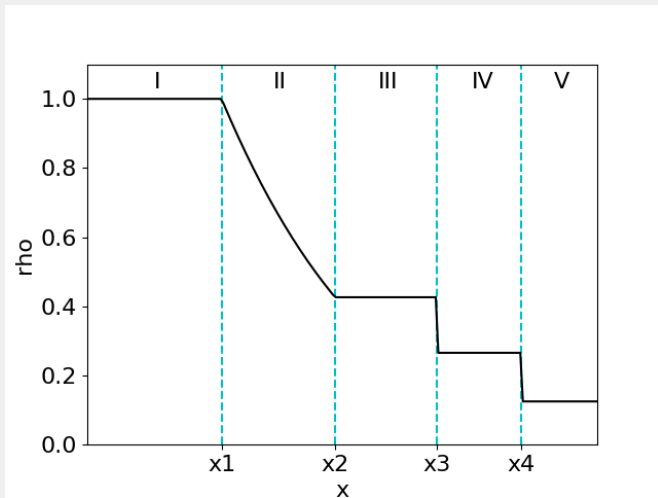


Figure 4: The exact solution of density at $t = 0.2$, with the ensuing fluid regions.

- BUT: OpenFOAM has variables p, U, \mathbf{T}
- Use ideal gas law to calculate value of T :

$$pV = nRT, \quad \rho = \frac{nM}{V} \quad \Rightarrow \quad T = \frac{pM}{\rho R} \quad (5)$$

$$\begin{pmatrix} p_L \\ U_L \\ T_L \end{pmatrix} = \begin{pmatrix} 1.0 \\ 0.0 \\ 3.484290 \times 10^{-3} \end{pmatrix}; \quad \begin{pmatrix} p_R \\ U_R \\ T_R \end{pmatrix} = \begin{pmatrix} 0.1 \\ 0.0 \\ 2.787432 \times 10^{-3} \end{pmatrix} \quad (6)$$

COMPARISON 2: SOD'S SHOCK TUBE

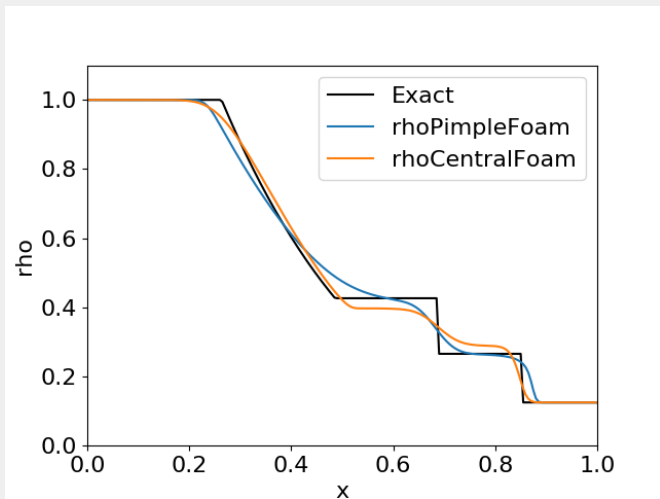


Figure 5: Comparison to exact solution of density at $t = 0.2$.

COMPARISON 2: SOD'S SHOCK TUBE

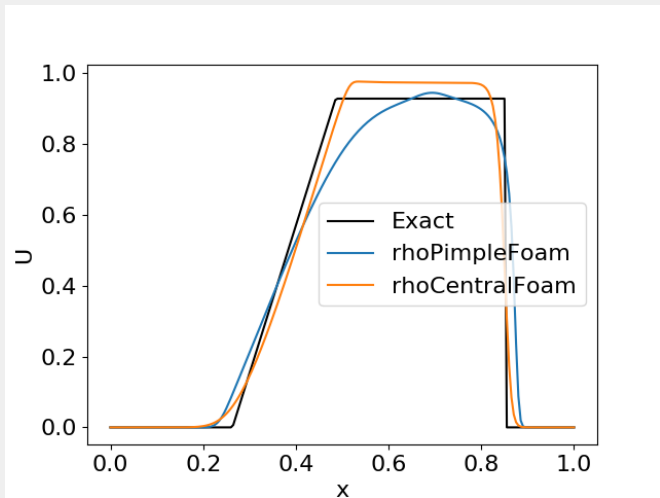
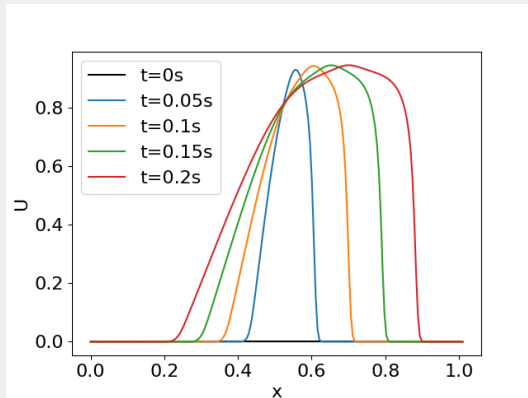
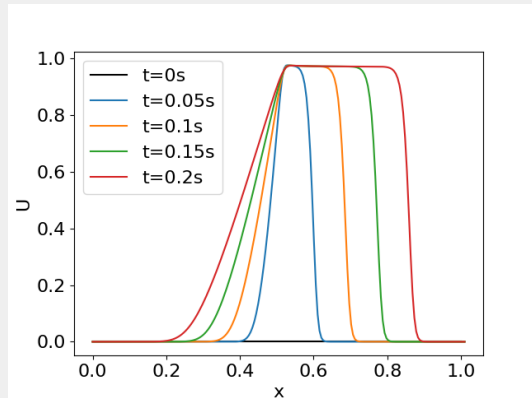


Figure 6: Comparison to exact solution of velocity at $t = 0.2$.

COMPARISON 2: SOD'S SHOCK TUBE



(a) rhoPimpleFoam



(b) rhoCentralFoam

Figure 7: Time evolution of the velocity solution from $t = 0$ to $t = 0.2$.

A more quantitative comparison metric, the L_1 norm:

$$L_1(Q^n, Q^*) = \frac{1}{Q_{ref}} \sum_{i=0}^{N=200} \left| Q^*\left(i \cdot \frac{1}{N}, n \cdot \Delta t\right) - Q_i^n \right| \quad (7)$$

Table 3: Normalized L_1 error norms of both numerical solutions

rhoPimpleFoam	t = 0.05	t = 0.1	t = 0.15	t = 0.2
p	1.9051	2.6689	3.3577	3.8180
ρ	1.7071	2.5219	3.2185	3.7374
U	4.7684	6.5525	8.3462	9.2785
T	2.7284	3.7757	4.8423	5.4644
rhoCentralFoam	t = 0.05	t = 0.1	t = 0.15	t = 0.2
p	1.7272	2.3440	2.8524	3.3806
ρ	1.6435	2.4459	3.1280	3.7782
U	3.7053	4.9110	6.0614	7.1656
T	3.4495	5.6248	7.6288	9.5964

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- ▶ Predicts shock speed fairly well despite diffusion
- ▶ Predicts values before/after shocks quite well

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Table 4: Solver runtime

Runtime [s]	Oblique shock				Shock tube
rhoPimpleFoam	645.49	634.95	636.11	631.61	32.07
rhoCentralFoam	353.67	351.44	346.42	344.58	8.74
Speedup	183%	181%	184%	183%	367%

- Rocket simulations!
- Impact on drag coefficients
- Detailed study of time evolution of errors
- Detailed study of run-time performance

THANK YOU FOR YOUR ATTENTION!